Please to	me a nhis	sion (+)	inside this	hov ->	

PTO/SB/05 (12/97)
Approved for use through 09/30/00. OMB 0651-0032

Patent and Trademark Office: U.S. DEPARTMENT OF COMMERCE
Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control

### UTILITY

#### PATENT APPLICATION TRANSMITTAL

(Only for new nonprovisional applications under 37 CFR 1.53(b))

orney Docket No.	20676-712	Total Pages	45
First No	amed Inventor or	Application Identi	ifier O
iver P. LEISTEN,	"An Antenna"		T <sub>P</sub>
oress Mail Label No.	EM08931082	8 US	s. 486

See MI	APPLICATION ELEMI EP chapter 600 concerning utility pater		AD	DRESS TO:	Assistant Commission Box Patent Applicatio Washington, DC 2023	n	09/2
2. [X]	Fee Transmittal Form (Submit an original, and a duplicate fo Specification (preferred arrangement set forth below - Descriptive title of the Invention - Cross References to Related Appl - Statement Regarding Fed sponsor - Reference to Microfiche Appendi - Background of the Invention - Brief Summary of the Invention - Brief Description of the Drawings - Detailed Description	[Total Pages 27] ) ications ed R&D	(if a,	eotide and/or opplicable, all a a Com b. Paper c. State  Assignment I	puter Readable Copy r Copy (identical to con ment verifying identify Papers (cover sheet & c	Submission  mputer copy)  of above cop  documents(s))	
	- Abstract of the Disclosure Drawing(s) (37 CFR 1.152)	[Total Sheets _2_]	9. [ ] 10. [ 1		(b) Statement s an assignee) Po by slation Document (if an		ey
	Oath or Declaration	[Total Pages _2_]	11.[]				
	a. [ ] Newly executed (original o	г сору)	12. [ X]		Amendment (10 pages)		
a. [ ] Newly executed (original or copy) b. [ X] Copy from a prior application (37 CFR 1.63(d)) (for continuation/divisional with Box 17 completed) [Note Box 5 below] i. [ ] DELETION OF INVENTOR(S) Signed statement attached deletting inventor(s) named in the prior application, see 37 CFR 1.63(d)(2) and 1.33(b).  5. [ X] Incorporation By Reference (useable if Box 4 bis checked) The entire disclosure of the prior application, from which a copy of the cost or declaration is supplied under Box 4b, is considered as being part of the disclosure of the accompanying application and is hereby incorporated by reference therein.				(Should be sp. Small Entity Statement(s) Certified Cop (uf foreign pr. Other:	pt Postcard (MPEP 50) eccifically itenized) Statement filed States still prop by of Priority Documen tority is claimed)	in prior appli per and desire at(s)	
i i	Continuation [ ] Divisional	[ ] Continuati			of prior application No. 0		
۳	, L 3	16. CORRESPO		·			
☐ Cus	tomer Number of Bar Code Label		021971		or [ X ] Correspo	ondence addre	ess below
NAME							
ADDR.	ESS						
CHANN		Tom one			lam con al		
CITY	mp v	STATE			ZIP CODE		
COUN	IKI	TELEPHONE			FAX		

01

SUBMITTED BY Typed or Printed Name

George A. Willman

Reg. Number <u>41.378</u>

Date <u>December 3, 1998</u>

					_				0	· · · · · · · · · · · · · · · · · · ·	
					L					omplete if Known	
	F	ΞE.	TRA	NSMITTAL		ation Nu	umber		Unassigned		
					Filing	Date			Herewith		
		Note:	Effectiv	ve October 1, 1997.	First Named Inventor			Oliver P. LEISTE	EN		
	Pa			bject to annual revision.	Group Art Unit			Unknown			
				NT (\$) 1928.00	Examir	ner Nami	е		Unknown		
TOTAL A	MOU	NI OF	PAYMI	ENT (\$) 1928.00	Attorne	y Docke	t Numbe	er	20676-712		
	MET	HOD	OE D	YMENT (check one)	i			FFF (	CALCULATIO	M (continued)	
					<del>                                     </del>					. ,	
				ereby authorized to charge lit any over payments to:	3. AD	OITIO	VAL FE	ES			
	licate	10030	and crec	it any over payments to:		Entity					
Deposit Account	23-2	415 (20	0676-71	2)	Fee	Fee	Fee	Fee	-	e Description	Fee Paid
Number	=				Code	(\$)	Code	(\$)			reeraiu
Deposit Account	Wils	on Son	sini Go	odrich & Rosati	105 127	130 50	205 227		Surcharge - late	ning ree or oath provisional filing fee or	
Name					1				cover sheet		
_					139	130	139		Non-English spe		<u> </u>
x Ch	arge A	kny Addi uired Ur	tional	Charge the Issue Fee Set in 37 CFR 1.18 at the Mailing of the Notice of Allowance	147	2,520	147			est for reexamination	
37	CFR	1.16 and	1.17	the Notice of Allowance	112	920*	112	920*	Requesting publi Examiner action	ication of SIR prior to	
2. X Pa	ymen		sed: Check	Money X Other	113	1,840*	113	1,840*	Requesting publi Examiner action	ication of SIR after	
	-	FI	EE CA	LCULATION	115	110	215	55	Extension for rep	oly within first month	
1. FILIN	VG F	EE			116	400	216	200	Extension for re	oly within second mont	h
					117	950	217	475	Extension for re	oly within third month	
Large Er	ntity =ee	Small	Fee		118	1,510	218	755	Extension for re	oly within fourth month	
	(\$)	Code	(\$)	Fee Description Fee Paid	128	2,060	228	1,030	Extension for re	oly within fifth month	
	790	201	395	Utility filing fee 790.00	119	310	219	155	Notice of Appea		
	330	206	165	Design filing fee	120	310	220			upport of an appeal	
	540	207	270	Plant filing fee	121	270	221	135	Request for oral		
	790	208	395	Reissue filing fee	138	1.510	138	1,510		ite a public use procee	dino
	150	214	75	Provisional filing fee	140	110	240	55	Petition to revive		
11-4	100	214									
			SUI	STOTAL (1) (\$) 790.00	141	1,320	241	660	Petition to revive		
				Fee from	142	1,320	242	660	Utility issue fee		-
2. CLA				Extra below Fee Paid		450	243	225	Design issue fe	9	
Total Clai		55	- 20 =	35 X 22 = 770.00	144	670	244	335	Plant issue fee		
Independ Claims	ient	7	- 3=	4 X 82 = 328.00	. 122	130	122	130	Petitions to the	Commissioner	
Multiple E	Depen	dent C	aims	0 X 270 = 0.00	123	50	123	50	Petitions related	to provisional applicat	ions
· ·					126	240	126	240	Submission of I	nformation Disclosure	Stmt
Large E	ntity Fee	Small Fee	Entity Fee		581	40	581	40	Recording each property (times	patent assignment per number of properties)	40.00
Code	(\$)	Code	(\$)	Fee Description	146	790	246	395		sion after final rejection a))	
103	22	203	11	Claims in excess of 20	1	me-	0.45	007			
102	82	202	41	Independent claims in excess of 3	149	790	249	395	examined (37 C	nal invention to be FR 1.129(b))	1
	270	204	135	Multiple dependent claim	1						
109	82	209	41	Reissue independent claims over original patent	Otho	er fee (sp	necify)	25	Request for Co.	rected Filing Receipt	i
110	22	210	11	Reissue claims in excess of 20	Care	ii icc (sp			11040001101 00	TOTOR I MING INCOCIDE	
l				and over original patent	Othe	er fee (sp	ecify)				
			SU	BTOTAL (2) (\$) 1,098.00	]	duced by	y Basic F	iling Fe	e Paid S	UBTOTAL (3)(\$)	40.00
SUBMIT	TED	вү								Complete (if a	applicable)
Typed or Printed N			orge A.	Willman						Reg. Number	41,378
		-	0	0	/,			Ι		Deposit Account	23-2415
Signature	e		/4	range WIL	<u>ı —</u>			Date	Dec. 3, 1998		(20676-712)

Burden Hour Statement: This form is estimated to take 0.2 hours to complete. Time will vary depending upon the needs of the individual case. Any comments on the amount of time you are required to complete this form should be sent to the Chief information Officer, Patient and Trademark Office, Washington, DC 20231. DO NOT SEXD FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Assistant Commissioner for Patients, Washington, DC 20231.

Attorney Docket No.: PATENT 20676.712

#### IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Application	)
Inventor: Oliver Paul Leisten	Group Art: Unknown
Application No.: Unassigned	
Filed: Herewith	Examiner: Unknown
Title: AN ANTENNA	
Which is a continuation of Application	
Serial No. 08/351,631	

Assistant Commissioner For Patents

Washington, D.C. 20231

Filed: December 6, 1994

Sir:

Applicant respectfully requests entry of this Preliminary Amendment.

#### In the Specification:

#### -- CONTINUING APPLICATION DATA

PRELIMINARY AMENDMENT

This application claims priority to United States Patent Application entitled An Antenna invented by Oliver Paul Leisten and having Application No. 08/351,631, filed on December 6, 1994, and which is incorporated herein by reference in its entirety.—;

#### In the Claims:

Please cancel claims 1-37 and add the following new claims 38-92:

- 38. (New) A radio telephone for use at frequencies greater than 200 MHz including an antenna which comprises an electrically insulative core of a solid material having a relative dielectric constant greater than 5, and a three-dimensional antenna element structure disposed on or adjacent the outer surface of the core and defining an interior volume, the material of the core occupying the major part of the said interior volume.
- 39. (New) A radio telephone according to claim 38, further comprising a feeder structure which is connected to the antenna element structure and passes through the core.
  - 40. (New) A radio telephone according to claim 38, wherein: the core is cylindrical and has distal and proximal end faces, the antenna includes an axial feeder structure and

the antenna element structure comprises at least two antenna elements extending from one end face in the direction of the other, and radial elements on at least the said one end face connecting the antenna elements to the feeder structure.

- 41. (New) A radio telephone according to claim 38, wherein the material of the core is ceramic and has a relative dielectric constant greater than 10.
- 42. (New) A radio telephone according to claim 38, having a feeder structure which passes through the core and is connected to the antenna element structure, wherein the core is solid with the exception of a central passage housing the feeder structure.
- 43. (New) A radio telephone according to claim 42, wherein the core is cylindrical, and has an axial extent at least as greater as its diameter, and with the diametrical extent of the solid material being at least 50 per cent of the said outer diameter.

- 44. (New) A radio telephone according to claim 38, wherein the core has a central axis and said antenna element structure comprises a plurality of antenna elements which are generally co-extensive in the axial direction.
- 45. (New) A radio telephone according to claim 38, wherein the core has a central axis and the antenna has a feeder structure extending through the core on the central axis, the antenna element structure comprising a plurality of antenna elements which are connected to the feeder structure at one end of the core and extend in the direction of the opposite end of the core to a common interconnecting conductor.
- 46. (New) A radio telephone according to claim 45, wherein the common interconnecting conductor forms a grounding conductor for the antenna element.
- 47. (New) A radio telephone according to claim 45, wherein the common interconnecting conductor is formed as a sleeve around a portion of the core.
  - 48. (New) A radio telephone according to claim 47, wherein the sleeve: is formed on an outer surface of the core and encircles the feeder structure; has a rim to which the said antenna elements are joined; and is connected to the feeder structure at the said opposite end of the core.
- 49. (New) A radio telephone according to claim 48, wherein the feeder structure has an inner conductor and a coaxial outer screen conductor, and wherein the sleeve is connected to the screen conductor.
- 50. (New) A radio telephone according to claim 45, wherein the antenna elements comprise helical tracks, and the sleeve is cylindrical.
  - 51. (New) A radio telephone according to claim 38, for handheld use.

- 52. (New) A radio telephone having an antenna the main resonant frequency of which is in excess of 500 MHz wherein the antenna comprises an electrically insulative antenna core of a material having a relative dielectric constant greater than 5, a three-dimensional antenna element structure disposed on or adjacent the outer surface of the core and defining an interior volume, and a feeder structure which is connected to the antenna element structure and passes through the core, the material of the core occupying the major part of the said interior volume.
- 53. (New) A radio telephone according to claim 52, wherein the antenna element structure comprises a plurality of antenna elements defining an envelope centered on a central longitudinal axis of the antenna, and wherein the feeder structure is coincident with the said axis.
- 54. (New) A radio telephone according to claim 53, wherein the core is a cylinder and the antenna elements define a cylindrical envelope which is coaxial with the core.
- 55. (New) A radio telephone according to claim 53, wherein the core is cylindrical and is solid with the exception of an axial passage housing the feeder structure.
- 56. (New) A radio telephone according to claim 55, wherein the volume of the solid material of the core is at least 50 per cent of the internal volume of the envelope defined by the elements, with the elements lying on an outer cylindrical surface of the core.
- 57. (New) A radio telephone according to claim 53, wherein the elements comprise metallic conductor tracks honded to the core outer surface.
- 58. (New) A radio telephone according to claim 52, wherein the material of the core is a ceramic.
- 59. (New) A radio telephone according to claim 58, wherein the relative dielectric constant of the material is greater than 10.

- 60. (New) A radio telephone according to claim 52, having a cylindrical core of solid material with an axial extent at least as great as its outer diameter, and with the diametrical extent of the solid material being at least 50 per cent of the outer diameter.
- 61. (New) A radio telephone according to claim 60, wherein the core is in the form of a tube having an axial passage of a diameter less than a half of its overall diameter, the inner passage having a conductive lining.
- 62. (New) A radio telephone according to claim 60, wherein the antenna element structure comprises a plurality of generally helical elements formed as metallic tracks on the outer surface of the core which are generally co-extensive in the axial direction.
- 63. (New) A radio telephone according to claim 62, wherein each helical element is connected to the feeder structure at one of its ends and to another of said helical elements at its other end.
- 64. (New) A radio telephone according to claim 63, wherein the connections to the feeder structure are made with generally radial conductive elements, and each helical element is connected to a ground or virtual ground conductor which is common to all of the helical elements.
- 65. (New) A radio telephone for operation at a frequency in excess of 200 MHz having an antenna which comprises a solid electrically insulative antenna core which has a central longitudinal axis and is made of a material having a relative dielectric constant greater than 5, a feeder structure extending through the core on the central axis, and, disposed on the outer surface of the core, a plurality of antenna elements which are connected to the feeder structure at one end of the core and extend in the direction of the opposite end of the core to a common interconnecting conductor.

- 66. (New) A radio telephone according to claim 65, wherein at least a portion of the core has a constant external cross-section in the axial direction, with the antenna elements being conductors plated on the surface of said portion.
- 67. (New) A radio telephone according to claim 66, wherein the antenna elements comprise a plurality of conductor elements extending longitudinally over the portion of the core having a constant external cross-section, and plurality of radial conductor elements connecting the longitudinally extending elements to the feeder structure at said one end of the core.
- 68. (New) A radio telephone according to claim 65, wherein the antenna includes an integral balun formed by a conductive sleeve extending over part of the length of the core from a connection with the feeder structure at the said opposite end of the core.
- 69. (New) A radio telephone according to claim 68, wherein the balun sleeve forms the common conductor for the longitudinally extending conductor elements, and wherein the feeder structure comprises a coaxial line having an inner conductor and an outer screen conductor, the conductive sleeve of the balun being connected at said opposite end of the core to the feeder structure outer screen conductor.
- 70. (New) A radio telephone according to claim 65, wherein the core is solid and has a cylindrical outer surface, and wherein the antenna elements comprise at least four longitudinally extending elements on the cylindrical outer surface and corresponding radial elements on a distal end face of the core connecting the longitudinally extending elements to the conductors of the feeder structure.
- 71. (New) A radio telephone according to claim 70, wherein the longitudinally extending elements are of different lengths.

- 72. (New) A radio telephone according to claim 71, wherein the antenna elements comprise four longitudinally extending elements, two of which are of greater length than the other two by virtue of following meandered paths on the outer surface of the core.
- 73. (New) A radio telephone according to claim 72, wherein each of the four longitudinally extending elements follow a respective generally helical path, the longer of the two elements each following a respective meandering course which deviates to either side of a helical center line.
- 74. (New) A radio telephone according to claim 70, wherein the radial elements are simple radial tracks which are all the same length.
- 75. (New) A telephone antenna comprising an electrically insulative core of a solid material having a relative dielectric constant greater than 5, and a three-dimensional antenna element structure disposed on or adjacent the outer surface of the core and defining an interior space, the material of the core occupying the major part of said interior space.
- 76. (New) An antenna for operation at frequencies in excess of 200 MHz, comprising an electrically insulative core of a solid material having a relative dielectric constant greater than 5, a three-dimensional antenna element structure disposed on or adjacent an outer surface of the core and defining an interior volume, and a feeder structure which passes through the core and provides an electrically balanced feed connection with the antenna element structure, the material of the core occupying the major part of said interior volume.
  - 77. (New) An antenna according to claim 76, including an integral balun.
- 78. (New) An antenna according to claim 77, wherein the balun includes a conductive layer on said outer surface of the core.

- 79. (New) An antenna according to claim 78, wherein said conductive layer comprises a conductive sleeve around part of the core, and wherein the, feeder structure comprises a coaxial combination of an inner conductor and an outer screen conductor, and wherein the sleeve is connected to said outer screen conductor.
- 80. (New) An antenna according to claim 79, wherein the core has a central axis and wherein said antenna element structure comprises a plurality of axially co-extensive antenna elements which extend from said balanced feed connection to a rim of the sleeve.
- 81. (New) An antenna according to claim 80, wherein the core is cylindrical and the antenna elements are helical.
- 82. (New) An antenna according to claim 80, wherein at least a portion of the core is of constant cross-section, centered on said axis, and wherein said antenna elements are located on an outer surface of said portion.
- 83. An antenna for operation at a frequency in excess of 200 MHz comprising: an antenna core in the form of an electrically insulative dielectric body made of a solid material having a dielectric constant greater than 5, wherein the body has an axis of symmetry and an outer surface directed outwardly from said axis, said outer surface enclosing an interior volume at least 50 per cent of which is occupied by said material,
  - a plurality of conductive antenna elements on said outer surface, a feeder connection for connecting the antenna elements to a feeder,
  - and an integral balun.
- 84. An antenna according to claim 83, including a coaxial feeder having an inner conductor and an outer screen, the feeder being surrounded by said dielectric body material, wherein the balun comprises a conductive layer on said outer surface spaced from said feeder by said material.

- 85. (New) An antenna according to claim 84, wherein the conductive layer is formed as a sleeve around part of the core, and wherein the feeder is located on said axis and passes through the core from said feeder connection to a second said connection, at which second connection said outer screen is connected to said sleeve.
- 86. (New) An antenna according to claim 85, wherein the sleeve has a rim spaced from said second connection and wherein the antenna elements extend in an electrically parallel connection from said feeder connection to said rim.
- 87. (New) An antenna for operation at a frequency in excess of 200 MHz comprising:
- an antenna core in the form of an electrically insulative dielectric body made of a solid material having a dielectric constant greater than 5, wherein the body has an axis of symmetry and an outer surface directed outwardly from said axis, said outer surface enclosing an interior volume at least 50 percent of which is occupied by said material,
  - a plurality of conductive antenna elements on said outer surface,
  - a feed connection, and
- a conductive sleeve formed on said outer surface and forming a cavity surrounding part of said dielectric body.
- 88. (New) An antenna according to claim 87, including a coaxial feeder having an inner conductor and an outer screen, the feeder being surrounded by said dielectric body material, wherein the sleeve comprises a conductive layer on said outer surface spaced from said feeder by said material.
- 89. (New) An antenna according to claim 87, wherein said dielectric body is a solid cylinder having first and second end surfaces, wherein one of said end surfaces is covered by a layer of conductive material, and wherein said sleeve is connected to said layer to form a cavity

which extends from said one end surface to a sleeve rim located on said body at a position intermediate said first and second ends.

- 90. (New) An antenna according to claim 89, further comprising a feeder, said cavity being connected to the feeder.
- 91. (New) An antenna according to claim 90, wherein the feeder is located on said axis and passes through the core from said feeder connection connecting the feeder to said antenna elements to a second connection, at which second connection said outer screen is connected to said conductive layer.
- 92. (New) An antenna according to claim 87, including a feeder, wherein the sleeve has a rim and wherein the antenna elements extend in an electrically parallel manner from said rim to a connection with the feeder.

#### REMARKS

It is asserted that no new matter is added by the foregoing Preliminary Amendment.

Prosecution in due course is respectfully requested.

Respectfully submitted,

WILSON SONSINI GOODRICH & ROSATI

Bv:

George A. Willman Reg. No. 41,378

650 Page Mill Road Palo Alto, California 94304 Telephone: (650) 493-9300 Date: December 3, 1998

#### AN ANTENNA

#### FIELD OF THE INVENTION

5

This invention relates to an antenna for operation at frequencies in excess of 200 MHz, and in particular to an antenna which has a three-dimensional antenna element structure.

10

#### BACKGROUND OF THE INVENTION

British Patent No. 2258776 discloses an antenna which has a three-dimensional antenna element structure by virtue of having a plurality of helical elements arranged around a common axis. Such an antenna is particularly useful for receiving signals from satellites, for example, in a GPS (global positioning system) receiver arrangement. The 20 antenna is capable of receiving circularly polarised signals from sources which may be directly above the antenna, i.e. on its axis, or at a location a few degrees above a plane perpendicular to the antenna axis and passing through the antenna, or from sources located anywhere in the solid angle between these extremes.

While being intended mainly for reception of circularly polarised signals, such an antenna, due to its three-dimensional structure, is also suitable as an 30 omnidirectional antenna for receiving vertically and horizontally polarised signals.

One of the disadvantages of such an antenna is that in certain applications it is insufficiently robust, and cannot 35 easily be modified to overcome this difficulty without a performance penalty. For this reason, antennas which are to receive signals from the sky in harsh environments, such as

on the outside of an aircraft fuselage, are often patch antennas, being simply plates (generally plated metallic square patches) of conductive material mounted flush on an insulated surface which may be part of the aircraft fuselage. However, patch antennas tend to have poor gain at low angles of elevation. Efforts to overcome this disadvantage have included using a plurality of differently oriented patch antennas feeding a single receiver. This technique is expensive, not only due to the numbers of elements required, but also due to the difficulty of combining the received signals.

#### SUMMARY OF THE INVENTION

15

According to one aspect of this invention an antenna for operation at a frequency in excess of 200 MHz comprises an electrically insulative antenna core of a material having a relative dielectric constant greater than 5, a three-20 dimensional antenna element structure disposed on or adjacent the outer surface of the core and defining an interior space, and a feeder structure which is connected to the element structure and passes through the core, the material of the core occupying the major part of the said 25 interior space.

Typically the element structure comprises a plurality of antenna elements defining an envelope centred on a feeder structure which lies on a central longitudinal axis. The 30 core is preferably a cylinder and the antenna elements preferably define a cylindrical envelope which is coaxial with the core. The core may be a cylindrical body which is solid with the exception of a narrow axial passage housing the feeder. Preferably, the volume of the solid material of 35 the core is at least 50 per cent of the internal volume of the envelope defined by the elements, with the elements lying on an outer cylindrical surface of the core. The

elements may comprise metallic conductor tracks bonded to the core outer surface, for example by deposition or by etching of a previously applied metallic coating.

5 For reasons of physical and electrical stability, the material of the core may be ceramic, e.g. a microwave ceramic material such as zirconium-titanate-based material, magnesium calcium titanate, barium zirconium tantalate, and barium neodymium titanate, or a combination of these. The 10 preferred relative dielectric constant is upwards of 10 or, indeed, 20, with a figure of 36 being attainable using zirconium-titanate-based material. Such materials have negligible dielectric loss to the extent that the Q of the antenna is governed more by the electrical resistance of the 15 antenna elements than core loss.

A particularly preferred embodiment of the invention has a cylindrical core of solid material with an axial extent at least as great as its outer diameter, and with the 20 diametrical extent of the solid material being at least 50 per cent of the outer diameter. Thus, the core may be in the form of a tube having a comparatively narrow axial passage of a diameter at most half the overall diameter of The inner passage may have a conductive lining 25 which forms part of the feeder structure or a screen for the feeder structure, thereby closely defining the radial spacing between the feeder structure and the antenna elements. This helps to achieve good repeatability in manufacture. This preferred embodiment has a plurality of 30 generally helical antenna elements formed as metallic tracks on the outer surface of the core which are generally coextensive in the axial direction. Each element is connected to the feeder structure at one of its ends and to a ground or virtual ground conductor at its other end, the 35 connections to the feeder structure being made with generally radial conductive elements, and the ground conductor being common to all of the helical elements.

According to another aspect of the invention, an antenna for operation at a frequency in excess of 200 MHz comprises a solid electrically insulative antenna core which has a central longitudinal axis and is made of a material having 5 a relative dielectric constant greater than 5, a feeder structure extending through the core on the central axis, and, disposed on the outer surface of the core, a radiating element structure comprising a plurality of antenna elements which are connected to the feeder structure at one end of 10 the core and extend in the direction of the opposite end of the core to a common grounding conductor. The core preferably has a constant external cross-section in the axial direction, with the antenna elements being conductors plated on the surface of the core. The antenna elements may 15 comprise a plurality of conductor elements extending longitudinally over the portion of the core having a constant external cross-section, and a plurality of radial conductor elements connecting the longitudinally extending elements to the feeder structure at the said one end of the 20 core. The phrase "radiating element structure" is used in the sense understood by those skilled in the art, that is to mean elements which do not necessarily radiate energy as they would when connected to a transmitter, and to mean, elements which either collect or radiate 25 electromagnetic radiation energy. Accordingly the antenna devices which are the subject of this specification may be used in apparatus which only receives signals, as well as in

30 In a particularly preferred embodiment of the invention, the antenna includes an integral balun formed by a conductive sleeve extending over part of the length of the core from a connection with the feeder structure at the above-mentioned opposite end of the core. The balun sleeve may thus also form the common grounding conductor for the longitudinally extending conductor elements. In the case of the feeder structure comprising a coaxial line having an inner

apparatus which both transmits and receives signals.

conductor and an outer screen conductor, the conductive sleeve of the balun is connected at the said opposite end of the core to the feeder structure outer screen conductor.

5 The preferred embodiment of the antenna, having a core which is a solid cylinder, includes an antenna element structure comprising at least four longitudinally extending elements the cylindrical outer surface of the core corresponding radial elements on a distal end face of the 10 core connecting the longitudinally extending elements to the conductors of the feeder structure. Preferably, these longitudinally extending antenna elements are of different In particular, in the case of an antenna having four longitudinally extending elements, two of the elements 15 are of greater length than the other two by virtue of following meandered paths on the outer surface of the core. In the case of an antenna for circularly polarised signals, all four elements follow a generally helical path, the longer of the two elements each following a meandering 20 course which deviates, preferably, sinusoidally on each side of a helical centre line. The conductor elements connecting the longitudinally extending elements to the feeder structure at the distal end of the core are preferably simple radial tracks which may be inwardly tapered.

25

Using the above-described features it is possible to make an antenna which is extremely robust due to its small size and due to the elements being supported on a solid core of rigid material. Such an antenna can be arranged to have the same 30 low-horizon omni-directional response as the prior art antenna which is mainly air-cored, but with robustness sufficient for use as a replacement for patch antennas in certain applications. Its small size and robustness render it suitable also for unobtrusive vehicle mounting and for use in handheld devices. It is possible in some circumstances even to mount it directly on a printed circuit board. Since the antenna is suitable for receiving not only

circularly polarised signals, but also vertically or horizontally polarised signals, it may be used not only in satellite navigation receivers but also in different types of radio communication apparatus such as handheld mobile telephones, an application to which it is particularly suited in view of the unpredictable nature of the received signals, both in terms of the direction from which they are received, and the polarisation changes brought about through reflection.

10

Expressed in terms of operating wavelength in air λ, the longitudinal extent of the antenna elements, i.e. in the axial direction, is typically within the range of from 0.03λ to 0.06λ, and the core diameter is typically 0.02λ to 0.03λ.
15 The track width of the elements is typically 0.0015λ to 0.0025λ, while the deviation of the meandered tracks from a helical mean path is 0.0035λ to 0.0065λ on each side of the mean path, measured to the centre of the meandered track. The length of the balun sleeve is typically in the range of from 0.03λ to 0.06λ.

According a third aspect of the invention, there is provided an antenna for operation at a frequency in excess of 200 MHz, wherein the antenna comprises an antenna element 25 structure in the form of at least two pairs of helical elements formed as helices having a common central axis, a substantially axially located feeder structure having an inner feed conductor and an outer screen conductor with each helical element having one end coupled to a distal end of 30 the feeder structure and its other end connected to a common grounding conductor, and a balun comprising a conductive sleeve located coaxially around the feeder structure, the sleeve being spaced from the outer screen of the feeder structure by a coaxial layer of insulative material having 35 a relative dielectric constant greater than 5, with the proximal end of the sleeve connected to the feeder structure outer screen. Preferably, the axial length of the helical elements is greater than the length of the sleeve of the balun. The sleeve conductor of the balun may also form the common grounding conductor, with each helical element terminating at a distal edge of the sleeve. In an 5 alternative embodiment, the distal edge of the sleeve is open circuit, and the common grounding conductor is the outer screen of the feeder structure.

The invention also includes, from another aspect, a method of manufacturing an antenna as described above, comprising forming the antenna core from the dielectric material, and metallising the external surfaces of the core according to a predetermined pattern. Such metallisation may include coating external surfaces of the core with a metallismaterial and then removing portions of the coating to leave the predetermined pattern, or alternatively a mask may be formed containing a negative of the predetermined pattern, and the metallic material is then deposited on the external surfaces of the core while using the mask to mask portions of the core

so that the metallic material is applied according to the pattern.

A particularly advantageous method of producing an antenna 25 having a balun sleeve and a plurality of antenna elements forming part of a radiating element structure, comprises the steps of providing a batch of the dielectric material, making from the batch at least one test antenna core, and then forming a balun structure, preferably without any radiating element structure, by metallising on the core a balun sleeve having a predetermined nominal dimension which affects the frequency of resonance of the balun structure. The resonant frequency of this test resonator is then measured and the measured frequency is used to derive an adjusted value of the balun sleeve dimension for obtaining a required balun structure resonant frequency. The same measured frequency can be used to derive at least one

dimension for the antenna elements of the radiating element structure to give a required antenna elements frequency characteristic. Antennas manufactured from the same batch of material are then produced with a balun sleeve and 5 antenna elements having the derived dimensions.

#### BRIEF DESCRIPTION OF THE DRAWINGS

10 In the drawings:-

Figure 1 is a perspective view of an antenna in accordance with the invention:

15 Figure 2 is a diagrammatic axial cross-section of the antenna;

Figure 3 is a fragmentary perspective view of part of the antenna;

20

Figure 4 is a cut-away perspective view of a test resonator;

Figure 5 is a diagram of a test rig including the resonator of Figure 4; and

25

Figure 6 is a diagram of an alternative test rig.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

30

Referring to the drawings, a quadrifilar antenna in accordance with the invention has an antenna element structure with four longitudinally extending antenna elements 10A, 10B, 10C, and 10D formed as metallic conductor

35 tracks on the cylindrical outer surface of a ceramic core 12. The core has an axial passage 14 with an inner metallic lining 16, and the passage houses an axial feeder conductor 18. The inner conductor 18 and the lining 16 in this case form a feeder structure for connecting a feed line to the antenna elements 10A - 10D. The antenna element structure also includes corresponding radial antenna elements 10AR,
5 10BR, 10CR, 10DR formed as metallic tracks on a distal end face 12D of the core 12 connecting ends of the respective longitudinally extending elements 10A -10D to the feeder structure. The other ends of the antenna elements 10A - 10D are connected to a common grounding conductor 20 in the form
10 of a plated sleeve surrounding a proximal end portion of the core 12. This sleeve 20 is in turn connected to the lining 16 of the axial passage 14 by plating 22 on the proximal end face 12P of the core 12.

15 As will be seen from Figure 1, the four longitudinally extending elements 10A - 10D are of different lengths, two of the elements 10B, 10D being longer than the other two 10A, 10C by virtue of following a meandering course. this embodiment, intended for circularly polarised signals, 20 the shorter longitudinally extending elements 10A, 10C are simple helices, each executing a half turn around the axis of the core 12. On the other hand, the longer elements 10B, 10D each follow a respective meandering course which is sinusoidal in shape, deviating on either side of a helical 25 centre line. Each pair of longitudinally extending and corresponding radial elements (for example 10A, 10AR) constitutes a conductor having a predetermined electrical length. In the present embodiment, it is arranged that the total length of each of the element pairs 10A, 10AR; 10C, 30 10CR having the shorter length corresponds to a transmission delay of approximately 135° at the operating wavelength, whereas each of the element pairs 10B, 10BR; 10D, 10DR produce a longer delay, corresponding to substantially 225°. Thus, the average transmission delay is 180°, equivalent to 35 an electrical length of  $\lambda/2$  at the operating wavelength. The differing lengths produce the required phase shift conditions for a quadrifilar helix antenna for circularly

polarised signals specified in Kilgus, "Resonant Quadrifilar Helix Design", The Microwave Journal, Dec. 1970, pages 49-54. Two of the element pairs 10C, 10CR; 10D, 10DR (i.e. one long element pair and one short element pair) are connected at the inner ends of the radial elements 10CR, 10DR to the inner conductor 18 of the feeder structure at the distal end of the core 12, while the radial elements of the other two element pairs 10A, 10AR; 10B, 10BR are connected to the feeder screen formed by metallic lining 16. At the distal end of the feeder structure, the signals present on the inner conductor 18 and the feeder screen 16 are approximately balanced so that the antenna elements are connected to an approximately balanced source or load, as will be explained below.

The effect of the meandering of the elements 10B, 10D is that propagation of a circularly polarised signal along the elements is slowed in the helical direction compared with the speed of propagation in the plain helices 10A, 10C. The sealing factor by which the path length is extended by the meandering can be estimated using the following equation:

Path length factor = 
$$\left[\int_{0}^{2n\pi} \frac{\dot{\Phi}}{\cos\{\tan^{-1}[an\cos{(n\dot{\Phi})}]\}} d\dot{\Phi}\right]/2\pi$$

25 where:-

 $\boldsymbol{\varphi}$  is the distance along the centre line of the meandered track, expressed in radians;

 $\it a$  is the amplitude of the meandered path, also in 30 radians; and

n is the number of cycles of meandering.

With the left handed sense of the helical paths of the longitudinally extending elements 10A - 10D, the antenna has its highest gain for right hand circularly polarised signals.

If the antenna is to be used instead for left hand circularly polarised signals, the direction of the helices is reversed and the pattern of connection of the radial elements is rotated through 90°. In the case of an antenna 10 suitable for receiving both left hand and right hand circularly polarised signals, albeit with less gain, the longitudinally extending elements can be arranged to follow paths which are generally parallel to the axis. Such an antenna is also suitable for use with vertically and 15 horizontally polarised signals.

In the preferred embodiment, the conductive sleeve 20 covers a proximal portion of the antenna core 12, thereby surrounding the feeder structure 16, 18, with the material 20 of the core 12 filling the whole of the space between the sleeve 20 and the metallic lining 16 of the axial passage 14. The sleeve 20 forms a cylinder having an axial length  $l_{\rm g}$  as show in Figure 2 and is connected to the lining 16 by the plating 22 of the proximal end face 12P of the core 12. 25 The combination of the sleeve 20 and plating 22 forms a balun so that signals in the transmission line formed by the feeder structure 16, 18 are converted between an unbalanced state at the proximal end of the antenna to a balanced state at the axial position corresponding to the upper edge 20U of 30 the sleeve 20. To achieve this effect, the length  $l_{\mathrm{R}}$  is such that, in the presence of an underlying core material of relatively high relative dielectric constant, the balun has an electrical length of  $\lambda/4$  at the operating frequency of the antenna. Since the remainder of the feeder structure 35 16, 18, i.e. distally of the upper edge 20U of the sleeve 20, is embedded in the core material 12 and, to a lesser extent, since the annular space surrounding the inner conductor 18 is filled with an insulating dielectric material 17 having a relative dielectric constant greater than that of air, the feeder structure distally of the sleeve 20 has a short electrical length. Consequently, 5 signals at the distal end of the feeder structure 16, 18 are at least approximately balanced.

The antenna has a main resonant frequency of 500 MHz or greater, the resonant frequency being determined by the effective electrical lengths of the antenna elements and, to a lesser degree, by their width. The lengths of the elements, for a given frequency of resonance, is also dependent on the relative dielectric constant of the core material, the dimensions of the antenna being substantially reduced with respect to an air-cored similarly constructed antenna.

The preferred material for the core 12 is zirconiumtitanate-based material. This material has the above-20 mentioned relative dielectric constant of 36 and is noted also for its dimensional and electrical stability with varying temperature. Dielectric loss is negligible. The core may be produced by extrusion or pressing.

- 25 The antenna elements 10A 10D, 10AR 10DR are metallic conductor tracks bonded to the outer cylindrical and end surfaces of the core 12, each track being of a width at least four times its thickness over its operative length. The tracks may be formed by initially plating the surfaces 30 of the core 12 with a metallic layer and then selectively etching away the layer to expose the core according to a pattern applied in a photographic layer similar to that used for etching printed circuit boards. Alternatively, the metallic material may be applied by selective deposition or
- 35 by printing techniques. In all cases, the formation of the tracks as an integral layer on the outside of a

dimensionally stable core leads to an antenna having dimensionally stable antenna elements.

With a core material having a substantially higher relative 5 dielectric constant than that of air, e.g.  $\in$  36, an antenna as described above for L-band GPS reception at 1575 MHz typically has a core diameter of about 5mm and the longitudinally extending antenna elements 10A - 10D have a longitudinal extent (i.e. parallel to the central axis) of 10 about 8mm. The width of the elements 10A - 10D is about 0.3mm and the meandered elements 10B, 10D deviate from a helical mean path by about 0.9mm on each side of the mean path, measured to the centre of the meandered track. Typically, there are five complete sinusoidal cycles of 15 meander in each element 10B, 10D to produce the required 90° phase difference between the longer and shorter of the elements 10A - 10D. At 1575 MHz, the length of the balun sleeve 22 is typically in the region of 8mm or less. Expressed in terms of the operating wavelength  $\lambda$  in air, 20 these dimensions are, for the longitudinal (axial) extent of the elements 10A - 10D:  $0.042\lambda$ , for the core diameter: 0.026%, for the balun sleeve: 0.042% or less, for the track width: 0.002%, and for the deviation of the meandered tracks: 0.005%. Precise dimensions of the antenna elements 25 10A - 10D can be determined in the design stage on a trial and error basis by undertaking eigenvalue delay measurements until the required phase difference is obtained.

In general, however, the longitudinal extent of elements 10A 30 - 10D is between  $0.03\lambda$  and  $0.06\lambda$ , the core diameter between  $0.02\lambda$  to  $0.03\lambda$ , the balun sleeve between  $0.03\lambda$  to  $0.06\lambda$ , the track width between  $0.0015\lambda$  to  $0.0025\lambda$ , and the deviation of the meandered tracks between  $0.0035\lambda$  to  $0.0065\lambda$ .

35 As a result of the very small size of the antenna, manufacturing tolerances may be such that the precision with which the resonant frequency of the antenna can be

maintained is insufficient for certain applications. In these circumstances, adjustment of the resonant frequency can be brought about by removing plated metallic material from the core, e.g. by laser erosion of part of the balun sleeve 20 where it meets one or more of the antenna elements 10A - 10D as shown in Figure 3. Here, the sleeve 20 has been eroded to produce notches 28 on either side of the junction with the antenna element 10A to lengthen the element thereby reducing its resonant frequency.

10

core.

A significant source of production variations in resonant frequency is the variability of the relative dielectric constant of the core material from batch to batch. preferred method of manufacturing the antenna described 15 above, a small sample of test resonators is produced from each new batch of ceramic material, these sample resonators preferably each having an antenna core dimensioned to correspond to the nominal dimension of the core of the antenna and plated only with the balun, as shown in Figure 20 4. Referring to Figure 4, the test core 12T, in addition to having a plated balun sleeve 20T, also has a plated proximal face 12PT. The inner passageway 14T of the core 12T may be plated between the proximal face 12PT and the level of the upper edge 20UT of the balun sleeve 12T or, as is shown in 25 Figure 4, it may be plated over its whole length with a metallic lining 16T. The external surfaces of the core 12T distally of the balun sleeve 20T are preferably left unplated.

30 The core 12T is pressed or extruded from the ceramic material batch to nominal dimensions, and the balun sleeve is plated with a nominal axial length. This structure forms a quarter-wave resonator, resonating at a wavelength λ corresponding approximately to four times the electrical length of the sleeve 20T when fed at the proximal end of the passage 14T where it meets the proximal end face 12PT of the

Next, the resonant frequency of the test resonator is measured. This can be performed as shown diagrammatically in Figure 5 by taking a network analyzer 30 and coupling its swept frequency source 30S to the resonator, here shown by 5 the reference numeral 32T, using, for example, a coaxial cable 34 with the outer screen removed over the length of a short end portion 34E. End portion 34E is inserted in the proximal end of the passage 14T (see Figure 4) with the outer screen of cable 34 connected to the metallised layer 10 16T adjacent the proximal face 12PT of the core 12T, and with the inner conductor of the cable 34 lying approximately centrally in the passage 14T to provide capacitive coupling of the swept frequency source inside the passage 14T. Another cable 36, with its end portion 36E having the outer 15 screen similarly cut back, is connected to the signal return 30R of the network analyzer 30 and is inserted in the distal end of the passage 14T of the core 12T. analyzer 30 is set to measure signal transmission between source 30S and return 30R and a characteristic discontinuity 20 is observed at the guarter-wave resonant frequency. Alternatively, the network analyzer can be set to measure the reflected signal at the swept frequency source 30S using the single cable arrangement shown in Figure 6. Again, a resonant frequency can be observed.

The actual frequency of resonance of the test resonator depends on the relative dielectric constant of the ceramic material forming the core 12T. An experimentally derived or calculated relationship between a dimension of the balun sleeve 20T, for example, its axial length, on the one hand and resonant frequency on the other hand, can be used to determine how that dimension should be altered for any given batch of ceramic material in order to achieve the required resonant frequency. Thus, the measured frequency can be used to calculate the required balun sleeve dimension for all antennas to be made from that batch.

This same measured frequency, obtained from the simple test resonator, can be used to adjust the dimensions of the radiating element structure of the antenna, in particular the axial length of the antenna elements 10A - 10D plated on 5 the cylindrical outer surface of the core distally of the sleeve 20 (using reference numerals from Figures 1 and 2). Such compensation for variations in relative dielectric constant from batch to batch may be achieved by adjusting the overall length of the core as a function of the resonant 10 frequency obtained from the test resonator.

Using the above-described method, it may be possible, depending on the accuracy with which the frequency characteristics of the antenna are to be set, to dispense 15 with the laser trimming process described above with reference to Figure 3. Although it is possible to use a complete antenna as a test sample, the advantage of using a resonator as described above with reference to Figure 4, i.e. without a radiating element structure, is that a simple 20 resonance can be identified and measured in the absence of interfering resonances associated with the radiating structure.

The above-described balun arrangement of the antenna, being plated on the same core as the antenna elements, is formed simultaneously with the antenna elements, and being integral with the remainder of the antenna, shares its robustness and electrical stability. Since it forms a plated external shell for the proximal portion of the core 12, it can be used for direct mounting of the antenna on a printed circuit board, as shown in Figure 2. For example, if the antenna is to be end-mounted, the proximal end face 12P can be directly soldered to a ground plane on the upper face of a printed circuit board 24 (shown in chain lines in Figure 2). With the inner feed conductor 18 passing directly through a plated hole 26 in the board for soldering to a conductor track on the lower surface. Since the conductor sleeve 20

35

is formed on a solid core of material having a high relative dielectric constant, the dimensions of the sleeve to achieve the required 90° phase shift are much smaller than those of an equivalent balun section in air. The sleeve 20 also has the effect of extending the ground up to the level of the upper edge 20U where it is used for grounding the antenna elements 10A - 10D, without intervening connecting elements.

It is possible within the scope of the invention to use alternative balun and feeder structures. For example, the feeder structure may have associated with it a balun mounted at least partly externally of the antenna core 12. Thus, a balun can be effected by dividing a coaxial feeder cable into two coaxial transmission lines acting in parallel, one 15 being longer than the other by an electrical length of 1/2, the other ends of these parallel-connected coaxial transmission lines having their inner conductors connected to a pair of inner conductors passing through the passageway 14 of the core 12 to be connected to respective pairs of the 20 radial antenna elements 10AR, 10DR; 10BR, 10CR.

As another alternative, the antenna elements 10A - 10D can be grounded directly to an annular conductor at the proximal edge of the cylindrical surface of the core 12, a balun 25 being formed by an extension of the feeder structure having a coaxial cable formed into, for example, a spiral on the proximal end face 12P of the core, so that the cable spirals outwardly from the inner passage 14 of the core to meet the annular conductor at the outer edge of the end face 12P 30 where the screen of the cable is connected to the annular conductor. The length of the cable between the inner passageway 14 of the core 12 and the connection to the annular ring is arranged to be \(\lambda/4\) (electrical length) at the operating frequency.

All of these arrangements configure the antenna for circularly polarised signals. Such an antenna is also

sensitive to both vertically and horizontally polarised signals, but unless the antenna is specifically intended for circularly polarised signals, the balun arrangement can be omitted. The antenna may be connected directly to a simple 5 coaxial feeder, the inner conductor of the feeder being connected to all four radial antenna elements 10AR - 10DR at the upper face of the core 12, and the coaxial feeder screen being coupled to all four longitudinally extending elements 10A - 10D via radial conductors on the proximal face 12P of 10 the core 12. Indeed, in less critical applications, the 10A -10D need not be helical in their configuration, but it is merely sufficient that the antenna element structure as a whole, comprising the elements and their connections to the feeder structure, should be a 15 three-dimensional structure so as to be responsive to both vertically and horizontally polarised signals. possible, for example, to have an antenna element structure comprising two or more antenna elements each with an upper radial connecting portion as in the illustrated embodiment, 20 but also with a similar lower radial connecting portion and with a straight portion connecting the radial portions, parallel to the central axis. Other configurations are This simplified structure is particularly applicable for cellular mobile telephony. 25 advantage of the antenna for handheld mobile telephones is that the dielectric core largely avoids detuning when the antenna is brought close to the head of the user. This is in addition to the advantages of small size and robustness.

As for the feeder structure within the core 12, in some circumstances it may be convenient to use a pre-formed coaxial cable inserted inside the passage 14, with the cable emerging at the end of the core opposite to the radial selements 10AR to 10DR to make a connection with receiver circuitry, for example, in a manner other than by the direct connection to a printed circuit board described above with

reference to Fig. 2. In this case the outer screen of the cable should be connected to the passage lining 16 at two, preferably more, spaced apart locations.

- 5 In most applications the antenna is enclosed in a protective envelope which is typically a thin plastics cover surrounding the antenna either with or without an intervening space.
- 10 What is claimed is:-

- An antenna for operation at a frequency in excess of 200 MHz, comprising an electrically insulative antenna core of a material having a relative dielectric constant greater
   than 5, a three-dimensional antenna element structure disposed on or adjacent the outer surface of the core and defining an interior volume, and a feeder structure which is connected to the element structure and passes through the core, the material of the core occupying the major part of the said interior volume.
- 2. An antenna according to claim 1, wherein the antenna element structure comprises a plurality of antenna elements defining an envelope centred  $\sqrt[O]{a}$  central longitudinal axis of the antenna, and wherein the feeder structure is coincident with the said axis.
- An antenna according to claim 2, wherein the core is a cylinder and the antenna elements define a cylindrical 20 envelope which is coaxial with the core.
  - 4. An antenna according to claim 2, wherein the core is a cylindrical body which is solid with the exception of an axial passage housing the feeder structure.
- 5. An antenna according to claim 4, wherein the volume of the solid material of the core is at least 50 per cent of the internal volume of the envelope defined by the elements, with the elements lying on an outer cylindrical surface of 30 the core.
  - 6. An antenna according to claim 2, wherein the elements comprise metallic conductor tracks bonded to the core outer surface.

35

 An antenna according to claim 1, wherein the material of the core is a ceramic.

- 8. An antenna according to claim 7, wherein the relative dielectric constant of the material is greater than 10.
- 9. An antenna according to claim 1, having a cylindrical 5 core of solid material with an axial extent at least as great as its outer diameter, and with the diametrical extent of the solid material being at least 50 per cent of the outer diameter.
- 10 10. An antenna according to claim 9, wherein the core is in the form of a tube having an axial passage of a diameter less than a half of its overall diameter, the inner passage having a conductive lining.
- 15 11. An antenna according to claim 9, wherein the antenna element structure comprises a plurality of generally helical antenna elements formed as metallic tracks on the outer surface of the core which are generally co-extensive in the axial direction.

20

- 12. An antenna according to claim 11, wherein each helical element is connected to the feeder structure at one of its ends and to a ground or virtual ground conductor at its other end, and wherein the connections to the feeder structure are made with generally radial conductive elements, the ground conductor being common to all of the helical elements.
- 13. An antenna for operation at a frequency in excess of 200 MHz, comprising a solid electrically insulative antenna core which has a central longitudinal axis and is made of a material having a relative dielectric constant greater than 5, a feeder structure extending through the core on the central axis, and, disposed on the outer surface of the 35 core, a plurality of antenna elements which are connected to the feeder structure at one end of the core and extend in

the direction of the opposite end of the core to a common grounding conductor.

- 14. An antenna according to claim 13, wherein the core has 5 a constant external cross-section in the axial direction, with the antenna elements being conductors plated on the surface of the core.
- 15. An antenna according to claim 14, wherein the antenna 10 elements comprise a plurality of conductor elements extending longitudinally over the portion of the core having a constant external cross-section, and a plurality of radial conductor elements connecting the longitudinally extending elements to the feeder structure at the said one end of the
- 16. An antenna according to claim 15, including an integral balun formed by a conductive sleeve extending over part of the length of the core from a connection with the feeder 20 structure at the said opposite end of the core.
- 17. An antenna according to claim 16, wherein the balun sleeve forms the common grounding conductor for the longitudinally extending conductor elements, and wherein the 25 feeder structure comprises a coaxial line having an inner conductor and an outer screen conductor, the conductive sleeve of the balun being connected at the said opposite end of the core to the feeder structure outer screen conductor.
- 18. An antenna according to claim 13, wherein the core is a solid cylinder, and wherein the antenna elements comprise at least four longitudinally extending elements on the cylindrical outer surface of the core and corresponding tradial elements on a distal end face of the core connecting the longitudinally extending elements to the conductors of the feeder structure.

- 19. An antenna according to claim 18, wherein the longitudinally extending elements are of different lengths.
- 20. An antenna according to claim 19, wherein the antenna 5 elements comprise four longitudinally extending elements, two of which are of greater length than the other two by virtue of following meandered paths on the outer surface of the core.
- 10 21. An antenna according to claim 20, wherein each of the four longitudinally extending elements follow a respective generally helical path, the longer of the two elements each following a respective meandering course which deviates to either side of a helical centre line.

15

- 22. An antenna according to claim 18, wherein the radial elements are simple radial tracks which are all the same length.
- 20 23. An antenna according to claim 13, having a plurality of antenna element with a longitudinal extent in the range of from  $0.03\lambda$  to  $0.06\lambda$ , the core diameter being in the range of from  $0.02\lambda$  to  $0.03\lambda$ , where  $\lambda$  is the operating wavelength of the antenna in air.

25

- 24. An antenna according to claim 23 and claim 16, wherein the length of the balun sleeve is in the range of from  $0.03\lambda$  to  $0.06\lambda$ .
- 30 25. An antenna for operation at a frequency in excess of 200 MHz, comprising an antenna element structure in the form of at least two pairs of helical elements formed as helices having a common central axis, a substantially axially located feeder structure having an inner feed conductor and
- 35 an outer screen conductor with each helical element having one end coupled to a distal end of the feeder structure and its other end connected to a common grounding conductor, and

- a balun comprising a conductive sleeve located coaxially around the feeder structure, the sleeve being spaced from the outer screen of the feeder structure by a coaxial layer of insulative material having a relative dielectric constant 5 greater than 5, with the proximal end of the sleeve connected to the feeder structure outer screen.
- 26. An antenna according to claim 25, wherein the sleeve conductor of the balun forms the common grounding conductor,10 with each helical element terminating at a distal edge of the sleeve.
- 27. An antenna according to claim 25, wherein the distal edge of the sleeve is open circuit, and the common grounding 15 conductor is the outer screen of the feeder structure.
- 28. Radio communication apparatus having an antenna according to claim 13, wherein the antenna is mounted directly on a printed circuit board forming part of the 20 apparatus.
- 29. A method of manufacturing an antenna as claimed according to claim 13, comprising forming the antenna core from the dielectric material, metallising the external surfaces of the core according to a predetermined pattern.
- 30. A method according to claim 29, wherein the metallisation step includes coating the external surfaces of the core with a metallic material and removing portions of 30 the coating to leave the predetermined pattern.
- 31. A method according to claim 29, wherein the metallisation step includes forming a mask containing a negative of the said predetermined pattern and depositing a metallic material on the external surfaces of the core while using the mask to mask portions of the core so that the

metallic material is applied according to the predetermined pattern.

32. A method of manufacturing a plurality of antennas as 5 claimed in claim 16 comprising:-

providing a batch of the dielectric material;
making from the batch at least one test antenna core;
forming a balun structure by metallising on the core a
balun sleeve having a predetermined nominal dimension which
affects the frequency of resonance of the balun structure;
measuring the resonant frequency to derive an adjusted
value of the balun sleeve dimension for obtaining a required
balun structure resonant frequency, and to derive at least
one dimension for the antenna elements giving a required

- 15 antenna elements frequency characteristic; and manufacturing from the same batch of material a plurality of antennas with a balun sleeve and antenna elements having the derived dimensions.
- 20 33. A method according to claim 32, wherein the test core is cylindrical and is made with an axial passage, and the passage is metallised over a section thereof which is coextensive with the balun sleeve.
- 25 34. A method according to claim 32, wherein the test core is cylindrical and is made with an axial passage, and the passage is metallised over the whole of its length.
- 35. A method according to claim 33 or claim 34, wherein the 30 said sleeve dimension is its axial length.
  - 36. A method according to claim 33 or claim 34, wherein the said dimension for the antenna elements is the length of at least some of the antenna elements.
  - 37. A method according to claim 33 or claim 34, wherein the said dimension for the antenna elements is the axial extent

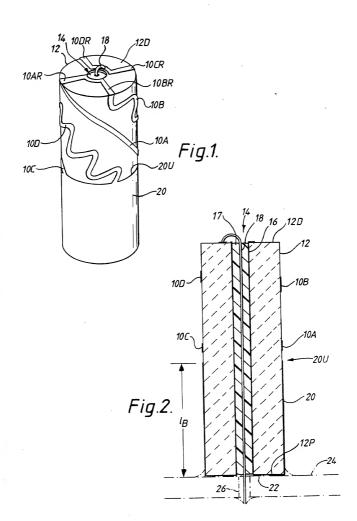
of the antenna elements, the said axial extent being the same for each of the antenna elements.

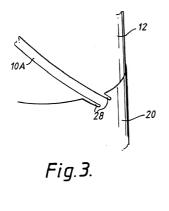
#### ABSTRACT OF THE DISCLOSURE

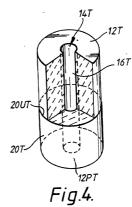
An antenna for use at UHF and upwards has a cylindrical ceramic core with a relative dielectric constant of at least A three-dimensional radiating element structure, consisting of helical antenna elements on the cylindrical surface of the core and connecting radial elements on a distal end face of the core, is formed by conductor tracks plated directly on the core surfaces. At the distal end 10 face the elements are connected to an axially located feed structure in a plated axial passage of the core. antenna elements are grounded on a plated sleeve covering a proximal part of the core which, in conjunction with the feeder structure, forms an integral balun for matching to an 15 unbalanced feeder.

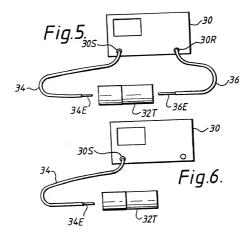
Since the ceramic core fills the major part of the interior volume defined by the radiating element structure, the antenna is very much smaller than an air-cored antenna. It

20 is also mechanically robust and electrically stable.









(Status)

# 

#### DECLARATION and POWER OF ATTORNEY

ORIGINAL
CONTINUATION
DIVISIONAL

as amended on \_

As a below named inventor, I declare that the information given herein is true, that I believe that I am the original, first and sole inventor if only one name is listed at 1 below, or a joint inventor if plural inventors are named below at 1-4, of the invention entitled;
AN ANTENNA
Which is described and claimed in:

(for declaration not accompanying application)
and for which a patent is sought, and that my residence, post office address and crizenship are as stated below next to my name.

I acknowledge my duty to disclose information which is material to the examination of this application in accordance with Title 37. Code of Federal Regulations §1.56(a).

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to

I hereby claim foreign priority benefits under Title 35, United States Code, § 119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filling date before that of the application on which priority is claimed:

COUNTRY	APPLICATION NUMBER	DATE OF FILING Month Day Year	PRIORITY CLAIMED UND 35 U.S.C. 119
UNITED KINGDOM	9417450.5	08 25 94	YES X NO

I hearty claim the benefit under Title 35, United States Code, \$720 of any United States application(s) isted below and, insofer as the subject matter of each of the claims of this application in or manner provided by the first paragraphs of Title 35, United States Code §171, assistanting the day to disclose material information as defined in Title 37, Code of Federal Regulations, \$1.56(a) which occurred between the filing date of the appreciation and the materiant of PCF international filing date of the application and the materiant of PCF international filing date of the application and the materiant of PCF international filing date of the applications.

(Application Senal No.) (Filing Date)

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorney(s) and/or Agent(s) to prosecute this application and transact all business in the Palent and Trademark Office connected therewith

MARTIN R. HORN, Reg. No. 18198, STUART LUBITZ, Reg. No. 2088; W. ROBERT SPENSLEY, Reg. No. 17433, RICHARD H. AZITLEN, Reg. No. 27248, JOHN LAND, Reg. No. 32584, ALEX CHARTOVER, Reg. No. 18192, WINCENT J. BELUSKO, Reg. No. 3028; ROS D. SERBOARA, Reg. No. 314001 M. SMON, Reg. No. 3258; ALEX M. FINKELSTEIN, Reg. No. 2108; WILLMAN K. KONRAD, Reg. No. 2848; CHOUNT SANDER, Reg. No. 31246, JOHN R. WETTERELR, Reg. No. 31489, ROCERT R. WINCENT, Reg. No. 2727; WILLMAN K. KONRAD, Reg. No. 22486; ROCERT R. WINCENT, NO. 2458; CHOUNT S. JOHN P. SCHERLACHER, Reg. No. 2009; CARY D. MANN, Reg. No. 3487; STACO'L HOWELLS, Reg. No. 3842; JUNE M. GOSTICH, Reg. No. 3138; CON P. LUCRINESE, Reg. No. 2240; WILLMAN K. KONRAD, Reg. No. 24586; CHOUNT S. CONTROLLED R. CONTROLL

Send correspondence to: SPENSLEY HORN JUBAS & LUBITZ 1880 Century Park East, Fifth Floor Los Angeles, California 90067

the specification in application Senat No.

DIRECT TELEPHONE CALLS TO: David M. Simon (310) 553-5050

(Please Print)

	Name		ME	FIRST NAME	MIDDLE NAME	Residence: CITY	STATE or COUNTRY
'	live!	LEIST	EN	OLIVER	PAUL	DUSTON	ENGLAND
	Post Office Address 90 WEGGS FARM RONNS 6HZ, ENGLAND				STON, NORTHAMP	TON,	CITIZENSHIP U.K.

2	Name of LAST NAME inventor	FIRST NAME	MIDDLE NAME	Residence: CITY	STATE or COUNTRY
	Post Office Address				CITIZENSHIP
3	Name of LAST NAME inventor	FIRST NAME	MIDDLE NAME	Residence: CITY	STATE or COUNTRY
	Post Office Address				CITIZENSHIP
4	Name of LAST NAME Inventor	FIRST NAME	MIDDLE NAME	Residence, CITY	STATE or COUNTRY
	Post Office Address				CITIZENSHIP

I further declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or impronoment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application or any patient issuing thereon.

SIGNATURE OF INVENTOR 1	SIGNATURE OF INVENTOR 2
28 th NOVEMBER 1994	DATE
SIGNATURE OF INVENTOR 3	SIGNATURE OF INVENTOR 4
DATE	DATE

 STATES PATENT	T AND TRADEMARK OFFICE

PATENT APPLICATION

IN RE PATENT APPLICATION OF	) Examiner: Ho. T.
Oliver P. Leisten	) Group Art Unit: 2514
Application No. 08/351,631	)
Filing Date: December 6, 1994	) }
Title: An Antenna	į

RECEIVED GROUP 2270

## POWER OF ATTORNEY BY ASSIGNEE TO EXCLUSION OF INVENTOR UNDER 37 C.F.R. § 3.71 WITH REVOCATION OF PRIOR POWERS

Commissioner of Patents and Trademarks Washington, D.C. 20231

Sir:

03/20/56

The undersigned ASSIGNEE of the entire interest in the above-identified application for letters patent hereby appoints Paul Davis, Reg. No. 29,294, Mark A. Haynes, Reg. No. 30,846, David J. Weitz, Reg. No. 38,362, Kent R. Richardson, Reg. No. 39,443, Charles C. Cary, Reg. No. 36,764, Michael J. Murphy, 37,404, George A. Willman, 41,378, Peter Eng. Reg No. 39,666, John Bruckner, Reg. No. 35,816, David Abraham, Reg. No. 39,554, and to prosecute this application and transact all business in the United States Patent and Trademark Office in connection therewith and hereby revokes all prior powers of attorney; said appointment to be to the exclusion of the inventors and the inventors' attorneys in accordance with the provisions of 37 C.F.R. § 3.71.

The following evidentiary documents establish a chain of title from the original owner to the Assignee:

- a copy of an Assignment attached hereto, which Assignment has been (or is herewith) forwarded to the Patent and Trademark Office for recording; or
- X the Assignment recorded on December 6, 1994, frames 7290/0389.

Pursuant to 37 C.F.R. § 3.73(b) the undersigned Assignee hereby states that evidentiary documents have been reviewed and hereby certifies that, to the best of ASSIGNEE's knowledge and belief, title is in the identified ASSIGNEE.

Direct all telephone calls to Mark A. Haynes at (415) 493-9300.

Address all correspondence to:

Mark A Haynes
WILSON SONSINI GOODRICH & ROSATI
A Professional Corporation
650 Page Mill Road
Palo Alto, CA 94304

ASSIGNEE: SYMMETRICOM, INC.

	(Signature)
Name:	William D. Rasdal
	(Print or Type)
Title: _	Chairman of the Board & CEO
Date:	December 2, 1997